

Changes in Mechanical Properties of Wood Due to 1 Year Outdoor Exposure¹

Gwang-Chul KIM^{2,†} · Jun-Ho KIM²

ABSTRACT

For quantitative evaluation of wooden structures, the mechanical performance of members has undergone outdoor exposure tests. A year-long monitoring was conducted using an SPF species. Test groups were divided into twelve (each month) to measure the moisture content, density and ultimate load. Starting from May when moisture content of the test group was at the lowest, simple failure modes were observed more frequently during the first half of the experiment, whereas complex failure modes took over during the second half. Starting from June when moisture content of the test group was the highest, ultimate load decreased by 30% in the second half compared to the first half. A multiple regression analysis confirmed that moisture content of the test group was the variable with most effect on ultimate load of various outdoor variables, and an estimation equation of a simple regression analysis revealed that moisture content and ultimate load formed an inversely proportionate relationship. It is thought that correlational relationships of variables other than moisture content could be applied with the increase in added data amount by longer periods of outdoor exposure tests.

Keywords: wooden structure, mechanical property, outdoor exposure test, ultimate load, regression analysis

1. INTRODUCTION

Wooden constructions tend to have better tolerance for earthquakes compared to other construction types. Numerous nailed joints and outer finishing materials, additional unstructured elements such as OSB, wooden constructions have more flexibility that can either absorb or release sudden lateral load energy in earthquakes. Moreover, wood as a material has a much stronger specific strength compared to steel or concrete, which enables weight lightening of the building, having strong resistance against lateral load (KBC, A, 2009). It can be predicted that the demand of wooden structures with

superior earthquake-resistant properties would rise, coupled with the current domestic situation, but there is hardly any research that quantitatively evaluates the safety of wooden structure that are directly related to consumers.

This study aims to build a database through an outdoor exposure test to explore the mechanical properties of wood exposed to open air. Data obtained from this study will be utilized not only in the quantitative evaluation of the safety of wooden structures but will also serve in manuals dealing with maintenance and repair.

¹ Date Received July 29, 2019, Date Accepted October 16, 2019

² Department of Housing Environmental Design, Chonbuk National University, Jeonju 54896, Republic of Korea

† Corresponding author: Gwang-Chul KIM (e-mail: gckim@jbnu.ac.kr, ORCID: 0000-0002-9774-0309)



Fig. 1. Measurement of moisture content and density.

2. MATERIALS and METHODS

An SPF (Spruce-Pine-Fir) that was kiln dried under 12% moisture content. The size of the test piece was 38×38×300(mm). Due to limited literature and previous studies on the mechanical properties of outdoor exposed wood, small test pieces instead of actual size , in order to obtain data (Kim *et al.*, 2011; Kim and Matsumura,

2013). The total number of test pieces in the study was 140, of which 20 were control groups and 120 were outdoor exposed for one year (10 pieces for each month) (Park *et al.*, 2018). The physical properties of the specimen were measured monthly before and after the test (Kim and Kim, 2019). The moisture content and density of the specimen were evaluated by cutting and drying two ends after the test (Han *et al.*, 2016).

The outdoor exposure test was conducted on the rooftop of the Chonbuk National University, College of Human Ecology, located in Jeonju City, Northern Jeolla Province. The test took place in the rooftop in order to maximize sunlight exposure on test pieces. The testing bench was made in accordance with the Weathering Testing Guidebook (McGreer, 2003), and was tilted at -5 degrees from level, in order to maximize reception of solar radiation through reflection and direct

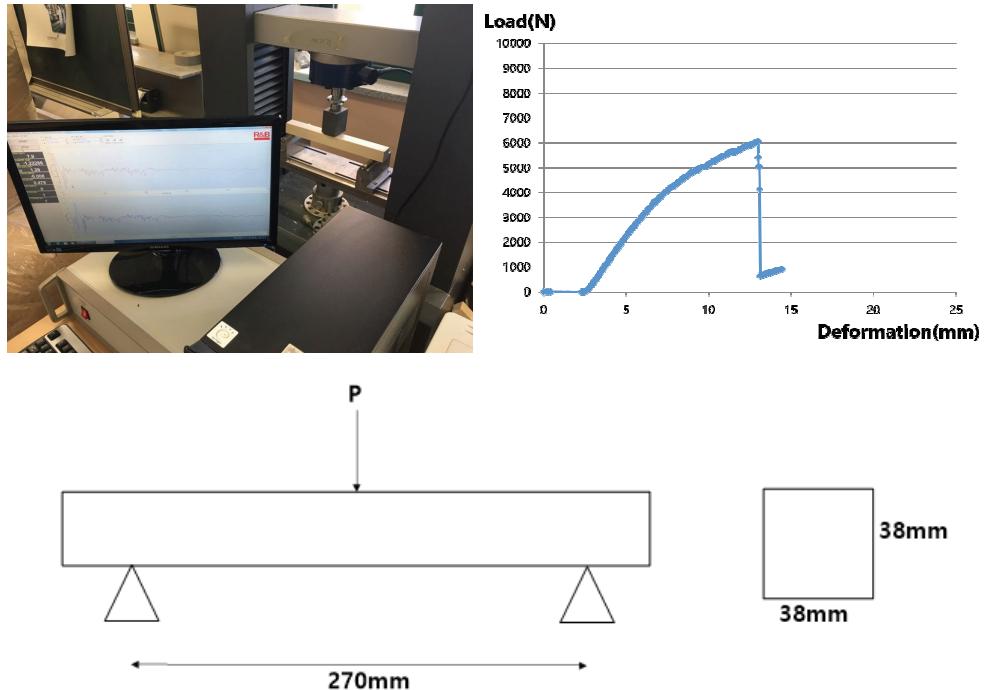


Fig. 2. The details for the bending test.

light at the testing (rooftop) environment with water-proof flooring. On-site temperature and humidity was measured daily at 2:00PM, and was recorded alongside data on the Korean National Weather Service web-site. In order to ensure all sides of the test pieces was evenly exposed to sunlight, all sides were turned over regularly (Kim and Kim, 2019; ASTM G7/G7M-13, 2013; ASTM G 90, 2005).

The bending test was carried out in three points, universal testing machine (10T) was used with the loading rate of 10mm/min (KS F 2150, 2014; Jung *et al.*, 2016; Sim and Kim, 2017). The span set to 270 mm. After the test, the failure figure of each test specimen was taken photographs, which were compared and contrasted with the eye to observe failure type (Kim, 2012). Failure modes were categorized into 6 types. The load-deformation curve was used for comparative analysis, exploring the mechanical performance depending on outdoor exposure time and moisture content change.

3. RESULTS and DISCUSSION

3.1. Failure mode analysis

Fig. 3 shows the failure modes categorized according to reference. According to reference, simple tension (ST) is not a common type in bending failure, but is a failure mode occasionally observed in high-density wood. Cross-grain tension (CT) is a typical failure form when the pressure put and the direction of the grain intersects. Splintering tension (SPT) is a collapse tensile failure that occurs mostly in wood with low moisture content, and Brash tension (BT) is a failure form that occurs in abnormal molecular structure wood that is easily broken. Compression (C) is a form that is typically found in zero-defect, low-density wood, and the Horizontal Shear (HS) is a type of failure that occurs in tree species that show drastic growth change. These are the six types categorized by the study (Jozsef, B. *et al.*, 1982).

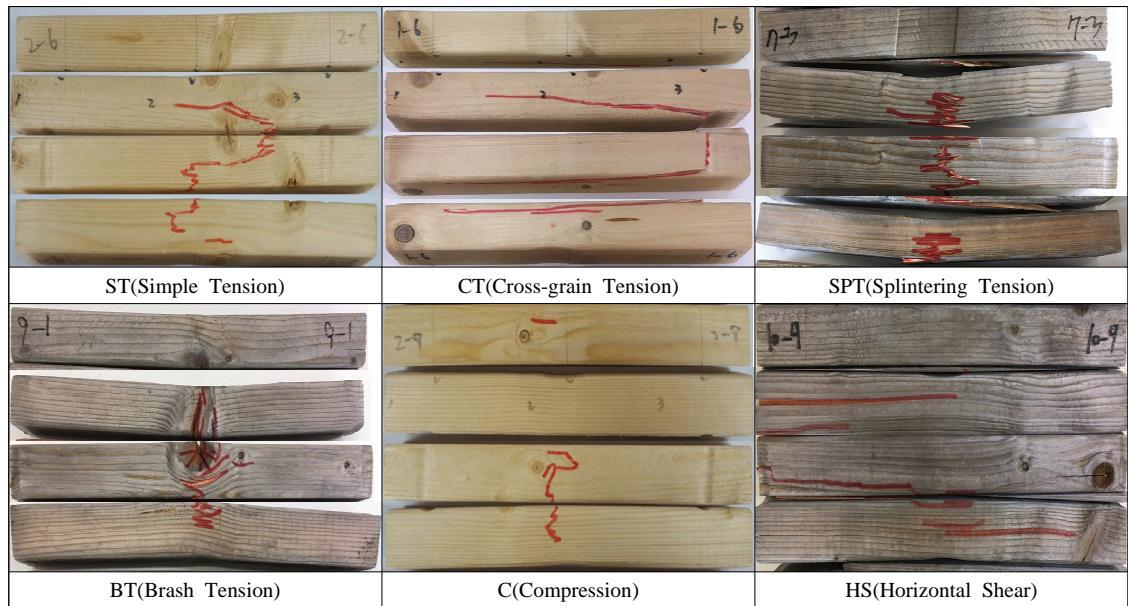


Fig. 3. Failure types.

Table 1. Failure type of specimen number

	C.g	1M	2M	3M	4M	5M	6M	7M	8M	9M	10M	11M	12M
No.1	ST	SPT	ST	BT	ST	SPT	ST	SPT	SPT	BT	CT	SPT	SPT
No.2	ST	CT	ST	ST	ST	SPT	ST	HS	SPT	HS	C	HS	SPT
No.3	C	HS	HS	C	HS	ST	SPT	SPT	SPT	HS	HS	SPT	SPT
No.4	ST	C	HS	ST	ST	SPT	HS	HS	SPT	HS	SPT	HS	C
No.5	ST	C	HS	ST	ST	SPT	SPT	SPT	ST	SPT	HS	SPT	HS
No.6	HS	CT	ST	SPT	ST	ST	SPT	SPT	C	SPT	C	SPT	SPT
No.7	C	ST	ST	HS	ST	SPT	SPT	SPT	HS	SPT	CT	CT	SPT
No.8	HS	HS	C	ST	ST	SPT	CT	CT	SPT	HS	C	CT	SPT
No.9	ST	CT	C	ST	ST	SPT	SPT	SPT	SPT	HS	SPT	SPT	SPT
No.10	ST	C	CT	ST	ST	HS	SPT	SPT	SPT	HS	ST	SPT	SPT

C.g : Control Group, M : Month, ST : Simple Tension, CT : Cross-grain tension,
SPT : Splintering Tension, BT : Brash Tension, C : Compression, HS : Horizontal Shear

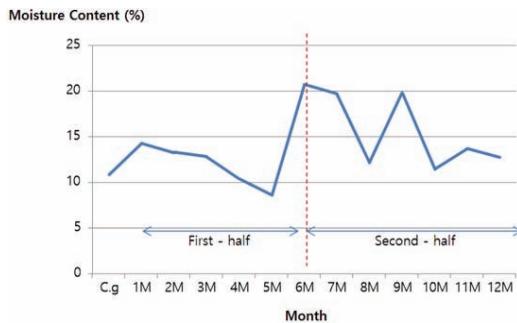
Table 2. Average of moisture content and density
(C.g: Control group, M: Month)

	Moisture Content (%)	Density (g / cm ³)
C.g	10.86(±0.23)	0.43(±0.07)
1M	14.29(±1.616)	0.45(±0.05)
2M	13.26(±0.5)	0.42(±0.03)
3M	12.78(±0.65)	0.41(±0.05)
4M	10.37(±0.47)	0.42(±0.03)
5M	8.59(±0.31)	0.39(±0.04)
6M	20.72(±2.04)	0.39(±0.03)
7M	19.69(±1.62)	0.42(±0.05)
8M	12.20(±0.78)	0.40(±0.05)
9M	19.83(±7.87)	0.45(±0.06)
10M	11.48(±1.57)	0.44(±0.05)
11M	13.72(±1.62)	0.43(±0.02)
12M	12.76(±0.9)	0.42(±0.06)

Fig. 3 categorizes failure modes of all test specimens with visual inspection. For test specimen that display two failure modes, the predominant mode was recorded. As shown in Table 1, the BT type was less considered in analysis as it is a failure mode mostly observed in abnormal molecular structures such as knots. Table 2 shows the moisture content and density of monthly test

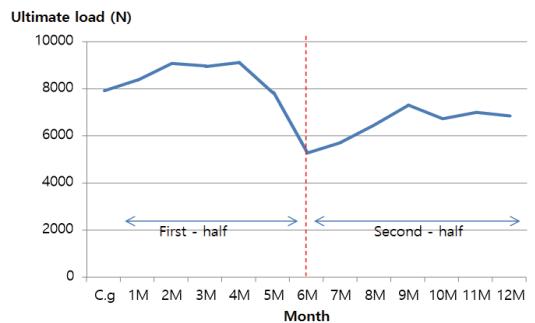
pieces and their control group. The average of the total density is 0.42(±0.019)g/cm³, which remained fairly consistent across all test pieces, and moisture contents showed similar or higher values than the control group except for May test specimen. May is a transitioning month between spring and summer in Korea with the largest daily range in the entire year, causing moisture content to shrink drastically compared to the control group.

In terms of failure mode, simple failures with little influence from outside factors such as ST, C, and HS types mainly occurred during January and April, when monthly moisture content showed little difference. However, the trend changed starting from May, the month with the test group's smallest moisture content of the year. Failure modes in the second half were predominantly complex failure SPT, failures that include the moisture content factor, rather than simple failure. The reason is thought to be the drastic change in moisture content from May to December, compared to previous months, thus having a critical influence on failure (Park and Kim, 2014; Yata S, 2001, Yu *et al.*, 2016). The line graph of moisture content in Fig. 4 shows a clear change in moisture content in the first and second halves.

**Fig. 4.** Comparison of moisture contents in 12 months.

3.2. Analysis for the ultimate load

The ultimate loads of monthly outdoor-exposed test pieces were averaged through a three-point bending load test. In order to reduce variation when measuring the average, the highest and lowest values were excluded from ultimate loads measured from 10 test specimen. As shown in Fig. 5, the lowest load value was observed in June when the moisture content was the highest of all 12 months at $20.72(\pm 2.04)\%$, as load is affected by moisture content. The average yearly load showed a general decrease starting from June. What should be

**Fig. 5.** Average of ultimate loads.

noted is the difference between ultimate loads of test groups with similar moisture content in both first and second halves of the test. Whereas the moisture content difference of test groups 2 month and 11 month, 3 month and 8 month is dismissible at 0.5%, the load plummeted from the first half of 2 and 3 months to the second half of 8 and 11 months by over 2000N. This is thought to be due to the breakup of a covalent bond (hemicellulose, lignin) that gives mechanical load to wood, as lignin is continuously decomposed by ultraviolet rays and washed away by rainfall, ultimately affecting load.

3.3. Verifying significance

As there were a total of 13 test groups (control + 12 months), an analysis of variance was conducted in order to compare more than two groups in order to verify the significance of ultimate loads of each group (Kim and Park, 2015a; Kim and Park, 2015b).

Results of the analysis of variance revealed a statistically significant change between ultimate loads of each group, as the F value exceeded its critical value and P value was smaller than 0.05. In other words, this experiment was appropriate, as 13 test group with different outdoor exposure times showed statistically significant difference in ultimate load. This allows us to assume that changes in outer factors due to differences in outdoor exposure time influenced the ultimate

Table 3. Average of ultimate loads.
(C.g: Control group, M: Month)

	Ultimate load (N)
C.g	7905.89(± 1378)
1M	8371.50(± 643)
2M	9075.44(± 411)
3M	8970.28(± 535)
4M	9140.61(± 838)
5M	7847.77(± 1459)
6M	5277.68(± 1144)
7M	5723.49(± 791)
8M	6465.30(± 921)
9M	7296.11(± 1390)
10M	6723.80(± 874)
11M	6993.27(± 871)
12M	6841.62(± 836)

Table 4. ANOVA table for the ultimate load**Summary**

Groups	Count	Sum	Average	Variance
Control Group	10	81679.55	8167.95	2168679
1 month	10	84270.97	8427.09	741714.3
2 month	10	94067.81	9406.78	595770.8
3 month	10	88098.04	8809.80	1885317
4 month	10	91662.68	9166.26	1233740
5 month	10	76967.49	7696.74	3320967
6 month	10	53676.4	5367.64	1569082
7 month	10	57143.3	5714.33	1092718
8 month	10	64258.78	6425.87	1142757
9 month	10	71224.66	7122.46	2987385
10 month	10	69408.42	6940.84	2376974
11 month	10	69270.8	6927.08	1114121
12 month	10	68083.2	6808.32	1675752

ANOVA

Source of variation	SS	DF	MS	F	P-value	F critical
Between groups	1.96E+08	12	16335577	9.69	7.12E-13	1.83
Within groups	1.97E+0.8	117	1684998			
	3.93E+08	129				

SS : Sum of Squares, DF : Degree of Freedom, MS : Mean Square

load of each test group.

3.4. Multiple regression analysis

A regression analysis was conducted to explore the correlations among obtained results. The dependent variable was set as the average ultimate load of each test group, and the independent variables were set as outdoor change factors including moisture content, daily range, highest and lowest temperature, rainfall and ultraviolet ray index. As there are more than one independent variable to describe the dependent variable, a multiple regression analysis was employed (Kim and Kim, 2016).

A multiple regression analysis of ultimate load and outdoor variables revealed that P values of all in-

dependent variables exceeded 0.05, making a statistically accurate analysis of correlation impossible. However, the influence of each independent variable was ascertainable. The P value of moisture content was relatively smaller than the P value of other variables, which led to a simple regression analysis only with the moisture content.

Results of the simple regression analysis showed statistically significant F and P values. An estimated equation on the correlational relationship between moisture content and ultimate load is as the following.

$$y = -188.53x + 10051.74 \quad (1)$$

y : Ultimate load (N), *x* : Moisture content (%)

Table 5. Multiple regression analysis**REGRESSION ANALYSIS STATISTIC**

MCC	0.81
R^2	0.66
M. R^2	0.33
SE	1021.41
COUNT	13

MCC : Multiple Correlation Coefficient, M. R^2 : Modify R^2 , SE : Standard Error**ANOVA**

	DF	SS	MS	F	Significant F
Regression	6	12562564	2093761	2	0.2
Within groups	6	6259716	1043286		
	12	18822279			

	C	SE	t	P-value	Low rank 95%	High rank 95%	Low rank 95.0%	High rank 95.0%
Y (Ultimate load)	10077.72	1599.12	6.3	0.0007	6164.81	13990.63	6164.81	13990.63
X 1 (Moisture content)	-182.58	90.51	-2.01	0.09	-404.07	38.9	-404.07	38.90
X 2 (Daily temperature range)	3308.77	2425.65	1.36	0.22	-2626.58	9244.13	-2626.58	9244.13
X 3 (Highest temperature)	-3376.71	2443.10	-1.38	0.21	-9354.77	2601.35	-9354.77	2601.35
X 4 (Lowest temperature)	3340.52	2469.12	1.35	0.22	-2701.22	9382.25	-2701.22	9382.25
X 5 (Rainfall)	-3.57	5.87	-0.6	0.56	-17.96	10.80	-17.96	10.80
X 6 (Ultraviolet index)	199.38	307.77	0.64	0.54	-553.71	952.47	-553.71	952.47

DF : Degree of Freedom, SS : Sum of Squares, MS : Mean Square, C : Coefficient

As the constant of the x value that represents moisture content in equation (1) is a negative, we know that ultimate load and moisture content is an inverse proportion. This indicates that the smaller the moisture content, the stronger the load.

As this study was only able to take a year-length

outdoor exposure test for statistical analysis, moisture content was the only variable among many outdoor variables that had a correlational relationship with ultimate load. More independent variables are expected to show correlation, however, as we amass more experimental data over additional 2 to 3 years.

Table 6. Simple regression analysis**REGRESSION ANALYSIS STATISTIC**

MCC	0.57
R^2	0.33
M. R^2	0.27
SE	1067.32
COUNT	13

MCC : Multiple Correlation Coefficient, M. R^2 : Modify R^2 , SE : Standard Error**ANOVA**

	DF	SS	MS	F	Significant F
Regression	1	6291222	6291222	5.52	0.03
Within groups	11	12531058	1139187		
	12	18822279			

	C	SE	t	P-value	Low rank 95%	High rank 95%	Low rank 95.0%	High rank 95.0%
Y (Ultimate load)	10051.74	1152.88	8.71	2.86E-06	7514.26	12589.21	7514.26	12589.21
X (Moisture content)	-188.534	80.22	-2.35	0.03	-365.11	-11.95	-365.11	-11.95

DF : Degree of Freedom, SS : Sum of Squares, MS : Mean Square, C : Coefficient

4. CONCLUSION

This study explored the mechanical properties of exposed to outdoor wood through an outdoor exposure test for quantitative evaluation of wooden structures. Existing mechanical performance evaluations on wooden buildings were predominantly non-destructive studies, but this study is noteworthy in that it directly destroyed members to acquire data.

This study presents the following conclusions.

1. The moisture content of all test groups generally showed moisture contents similar to or higher than that of the control group(10.86%), whereas the May test group showed the lowest value of 8.59%, due to the widest daily range.

2. In the first half of the experiment (January~April) when moisture content changes were relatively small, simple failure forms such as ST, C and HS constituted the majority of all failure forms. However, starting from May, the second half (June~December) produced predominantly complex failure forms such as SPT. This can be attributed to the increased fatigue of test pieces as a result of enduring fluctuations in moisture content that was higher in the second half compared to the first half.
3. Starting from June with the highest moisture content, the ultimate load average of June (20.72%) decreased by approximately 30% in the second half compared to the first half, which can be attributed to the decomposition of lignin in

- the wood by ultraviolet rays due to outdoor exposure.
4. A multiple regression analysis between various outdoor variables and ultimate load revealed that moisture content was the most influential.
 5. The experiment has progressed for only a year, but correlational relationships between other outdoor variables and ultimate loads are expected to change with longer experiment time.

ACKNOWLEDGMENT

This research was supported by Basic Science Research Program through the National Research Foundation of Korea (NRF) funded by the Ministry of Education (NRF-2016R1D1A3B03932199).

REFERENCES

- ASTM G7/G7M-13. 2013. Standard practice for atmospheric environmental exposure testing of nonmetallic materials. American Society for Testing and Materials(ASTM), West Conshohocken.
- ASTM G 90. 2005. Standard practice for performing accelerated outdoor weathering of nonmetallic materials using concentrated natural sunlight. American Society for Testing and Materials (ASTM), West Conshohocken.
- Forest Products Laboratory. 2010. Wood handbook: Wood as an engineering material. USDA Forest Service, Madison, Wisconsin.
- Han, Y.J., Lee, H.M., Eom, C.D. 2016. Physical and Mechanical Properties of Korean Red Pine Wood from Different Growth Sites and Correlations between Them. Journal of the Korean Wood Science and Technology 44(5): 695-704
- Jozsef, B., Benjamin, A.J. 1982. Mechanics of wood and wood composites. Van Nostrand Reinhold Company Inc CH 7.
- Jung, H.J., Song, Y.J., Lee, I.H., Hong, S.I. 2016. Lateral Load Performance Evaluation of Larch Glulam Portal Frames Using GFRP-Reinforced Laminated Plate and GFRP Rod. 2016. Journal of the Korean Wood Science and Technology 44(1): 30-39.
- KS F 2150. 2014. Method of Static Bending Test for Full Sized Structural Lumber. Korean Standards Association, Seoul.
- KBC, A. 2009. Korean building code-structural. Seoul, Korea: Architectural Institute of Korea.
- McGreer, M. 2003. Weathering Testing Guidebook. Chicago, USA: Atlas Electric Devices Company.
- Kim, G.C., Kang, C.W., Matsumura, J. 2011. A Study on the Bending Properties of Traditional Korean Joints. Journal of the Faculty of Agriculture, Kyushu University 56(2): 353-360.
- Kim, G.C. 2012. Study on the Change of Physical and Anatomical Properties in the Pine Wood by Accelerated Weathering Test. Korea Furniture Society 23(3): 324-331.
- Kim, G.C., Matsumura, J. 2013. Study on the change of bending performance for wood member by accelerated weathering test. Journal of the Faculty of Agriculture, Kyushu University 58(2): 351-357.
- Park, C.Y., Kim, G.C. 2014. Evaluation of Modulus of Elasticity of Wood Exposed to Accelerated Weathering Test by Measuring Ultrasonic Transmission Time. Journal of the Korean Wood Science and Technology 42(3): 275-281.
- Park, Y.G., Han, Y.J., Park, J.H., Chung, H.W., Kim, H.B., Chang, Y.S., Yeo, H.M. 2018. Evaluation of Deterioration of Larix kaempferi Wood Heat-treated by Superheated Steam through Field Decay Test for 12 Months. Journal of the Korean Wood Science and Technology 46(5): 497-510.
- Kim, G.C., Park, C.Y. 2015a. Analysis of Surface Color Characteristics of Wood in Accelerated Weathering Test. Korea Furniture Society 26(3): 262-266.
- Kim, G.C., Park, C.Y. 2015b. Mechanical Properties

Changes in Mechanical Properties of Wood Due to 1 Year Outdoor Exposure

- of Zelkova Serrata Makino in Accelerated Weathering Test. Korea Furniture Society 26(4): 392-397.
- Kim, G.C., Kim, J.H. 2016. Performance comparison of Korean tongue and groove joint between hand-made and pre-cut. Journal of the Korean Wood Science and Technology 44(5): 664-677.
- Kim, G.C., Kim, J.H. 2019. The Measurement of Physical Properties of Outdoor Exposed Members. Journal of the Korean Wood Science and Technology 47(3): 311-323.
- Sim, J.K., Kim, G.C. 2017. A Study on The Comparison of Mechanical Property Between The Staggered Stud Wood Wall and The Standard Wood Frame Wall. Journal of the Korean Wood Science and Technology 45(5): 640-649.
- Yata, S. 2001. Occurrence of drying checks in softwood during outdoor exposure. In: Imamura Y (ed) High-performance utilization of wood for outdoor uses. Wood Research Institute Kyoto University, Kyoto, pp. 65-70.
- Yu, S.G., Chang, S.J., Kang, Y.J., Kim, S.M. 2016. Comparison of Hygrothermal Performance between Wood and Concrete Wall Structures using Simulation Program. Journal of the Korean Wood Science and Technology 44(2): 283-293.